

L.S. Assetova, B.M. Nurlanova, I.A. Samoiloa

*Ye.A. Buketov Karaganda State University, Kazakhstan
(E-mail: b.nurlanova@mail.ru)*

Bending of the rigidly fixed elastic-plastic plate

The number of plate structures include coatings, as well as box systems, working as a complete spatial system. The plate structures include systems elements of which are both rods and plates, for example, frame-panel structures with the bearing capacity of frame-panel buildings when considering the theory of bending. In the theory of elastic-plastic plates, the algorithm of calculation according to this theory, its basic formulas, the basic relations of the theory of elasticity are considered. This article discusses the bending of the rigidly fixed elastic-plastic plate. Calculations were made using the method of separation of variables. This method was implemented in the program MathCAD. Values of the laws of stress and modulus of materials, bending functions, shear components, deformation components, bending moment values, torsion and internal forces, stresses are obtained and plots of distribution functions are plotted. The values of the distribution functions of the rigidly fixed elastic-plastic plate are determined.

Keywords: plate, elastic, plastic, malleability, bending, deformation, stress.

Introduction

Plates of flagstones are called elastic cylindrical or prismatic bodies thickness of which is small comparing with two others in the size. Plate is widespread in building: panels, ferro-concrete or slab, the bases of the big buildings, flagstones, etc. Depending on foundation plates differ: round, pillow-like, triangular, quadrangular and polygonal. At present, plates are used in many technical branches: in building, in aircraft, in ship building, at assemblage of cars. Plates are the important designs in different branches of technics and in building. Therefore plate predesign is very important. To make or use any construction predesign is necessary. As the plate is the main element of many constructions predesign of bending and bearing ability is the important problem. To determine regularity of change of internal forces of elastic-plastic plates. In the calculation of the elastic, plastic, elastic-plastic plates with different bearing on the bending deflections and compare distributed functions [1, 2].

Main part

Consider a rigid-reinforced elastic-plastic plate of rectangular shape in a Cartesian coordinate system (l_1, l_2, h – plate dimensions in the direction of the coordinate axes) (Fig. 1) [3–11].

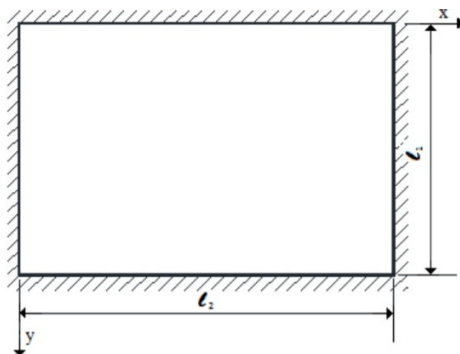


Figure 1. Rigidly fixed plate

Let it be acted q_0 on by a uniformly distributed load. The calculation is made using the method of separation of variables. This method will be implemented in the program MathCAD.

Given:

$$l_1 = 1, l_2 = 1, a_1 = 1, b_1 = 1, a_2 = 2, b_2 = 2, h = \frac{1}{2}, E_0 = 2 \cdot 10^5, \nu = \frac{1}{4}, q_0 = 1.$$

The boundary values of the parameters when rigidly fixed form will take the following form:

$$\alpha_0 = 0, \beta_0 = 0.$$

We calculate the dimensionless function of the plate bend:

$$f(x, y) = X(x) \cdot Y(y) = \frac{1}{24^2} (x^4 - 2x^3 + x^2) \cdot (y^4 - 2y^3 + y^2).$$

Bending parameters are defined as follows:

$$m = \frac{l_1}{l_2} = 1, I_1 = \frac{1}{720}, I_2 = 0, J_1 = \frac{1}{720}, J_2 = 0,$$

$$\alpha = \frac{1}{\frac{1}{m^2} \cdot J_1 + 2 \cdot I_2 \cdot J_2 + m^2 \cdot I_1} = 360.$$

Cylindrical plate stiffness:

$$D_0 = \frac{E_0 \cdot h^3}{12 \cdot (1 - \nu^2)} = \frac{20000}{9}.$$

The laws of stress and module functions of materials (Fig. 2):

$$\varphi(\xi) = \sin\left(\frac{\pi}{2} \cdot \xi\right), \quad \psi(\xi) = \frac{\sin\left(\frac{\pi}{2} \cdot \xi\right)}{\xi},$$

where ξ - deformation parameter.

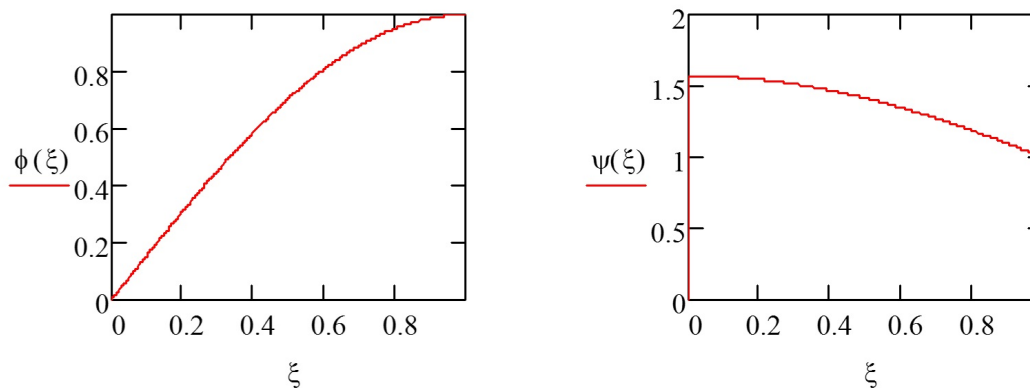


Figure 2. The laws of stress and module functions of materials

The value of the stress change laws and material functions of the module are shown in Table 1.

Table 1

The value of the stress change laws and functions of materials module

ξ	0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1
$\varphi(\xi)$	0	0.156	0.309	0.454	0.588	0.707	0.809	0.891	0.951	0.988	1
$\psi(\xi)$	0	1.564	1.545	1.513	1.469	1.414	1.348	1.273	1.189	1.097	1

Using dimensionless function of bending plates, as follows: define the great bend feature $W(x, y, \xi)$ (Fig. 3):

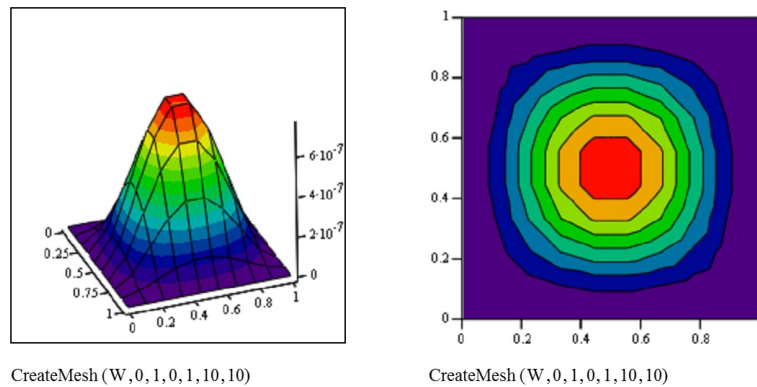


Figure 3. Bending function

Using the components of the shear, determine the strain components and their diagrams at $z = 0.5, \xi = 0.5$ (Fig. 4) [12]:

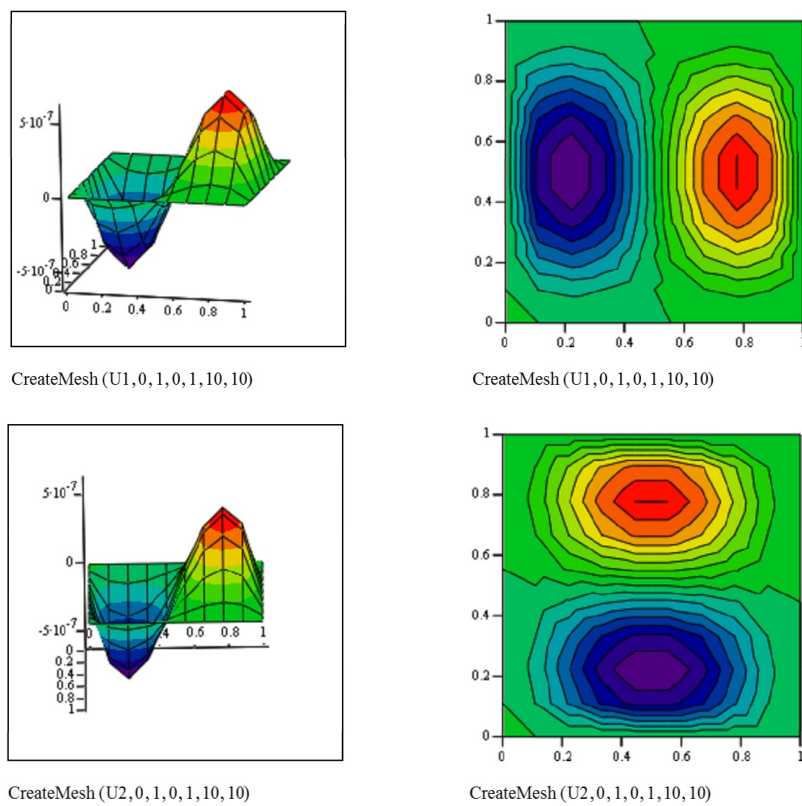


Figure 4. Shear components

Using shear components, we define the deformation components and their diagrams at $z = 0.5$ (Fig. 5) [13]:

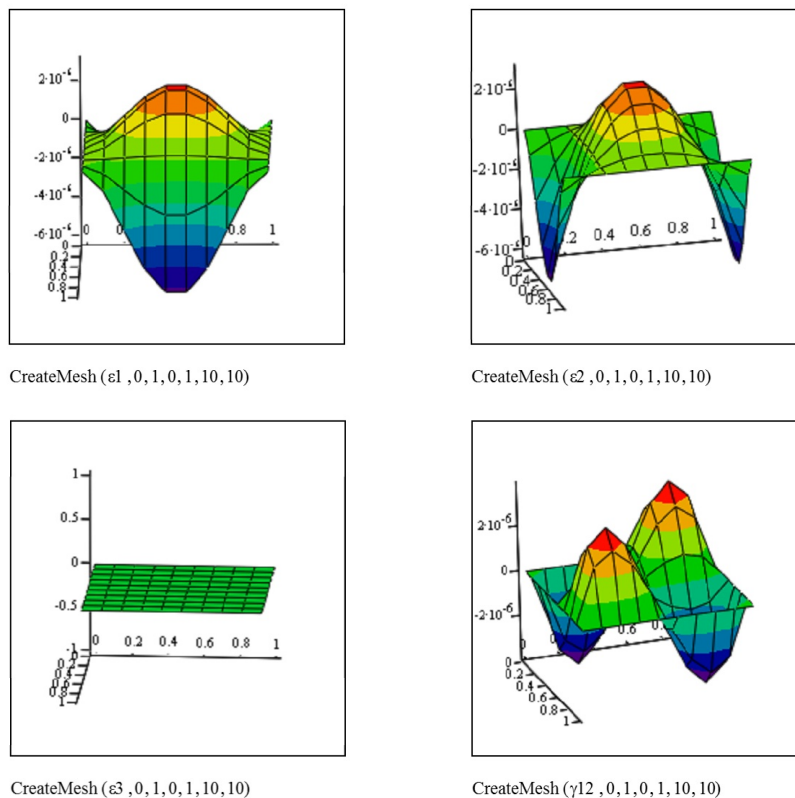
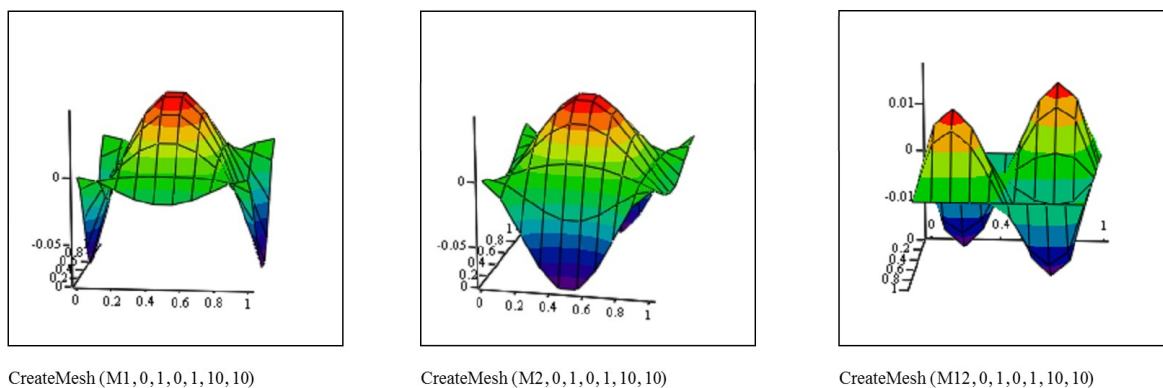


Figure 5. Deformation components

We calculate the internal forces (Fig. 6):

$$\bar{E}_0 = \frac{640000}{3}; \bar{E}(\xi) = \frac{640000 \cdot \sin\left(\frac{\pi \cdot \xi}{2}\right)}{3 \cdot \xi}; D(\xi) = \frac{20000 \cdot \sin\left(\frac{\pi \cdot \xi}{2}\right)}{9 \cdot \xi};$$

$$PU(x, y) = 1; q(x, y) = q_0 \cdot PU(x, y) = 1.$$



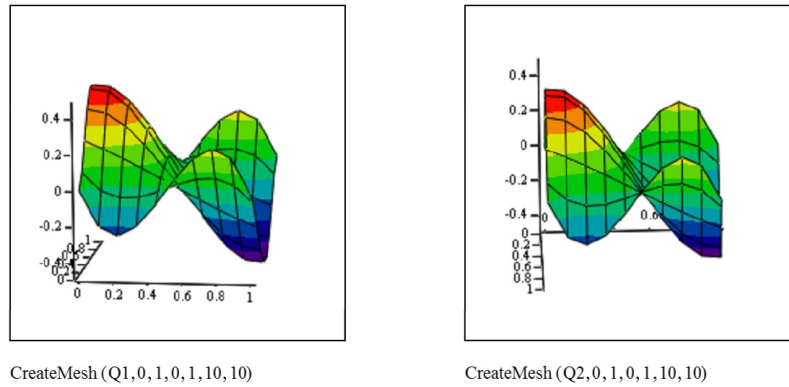


Figure 6. Moments of bending, torsion and internal forces

We find the components of stress, using the found internal forces [14–16]. At $x = 0.5$, $y = 0.5$ and $x = -0.5$, $y = -0.5$ and their diagrams are as follows (Fig. 7):

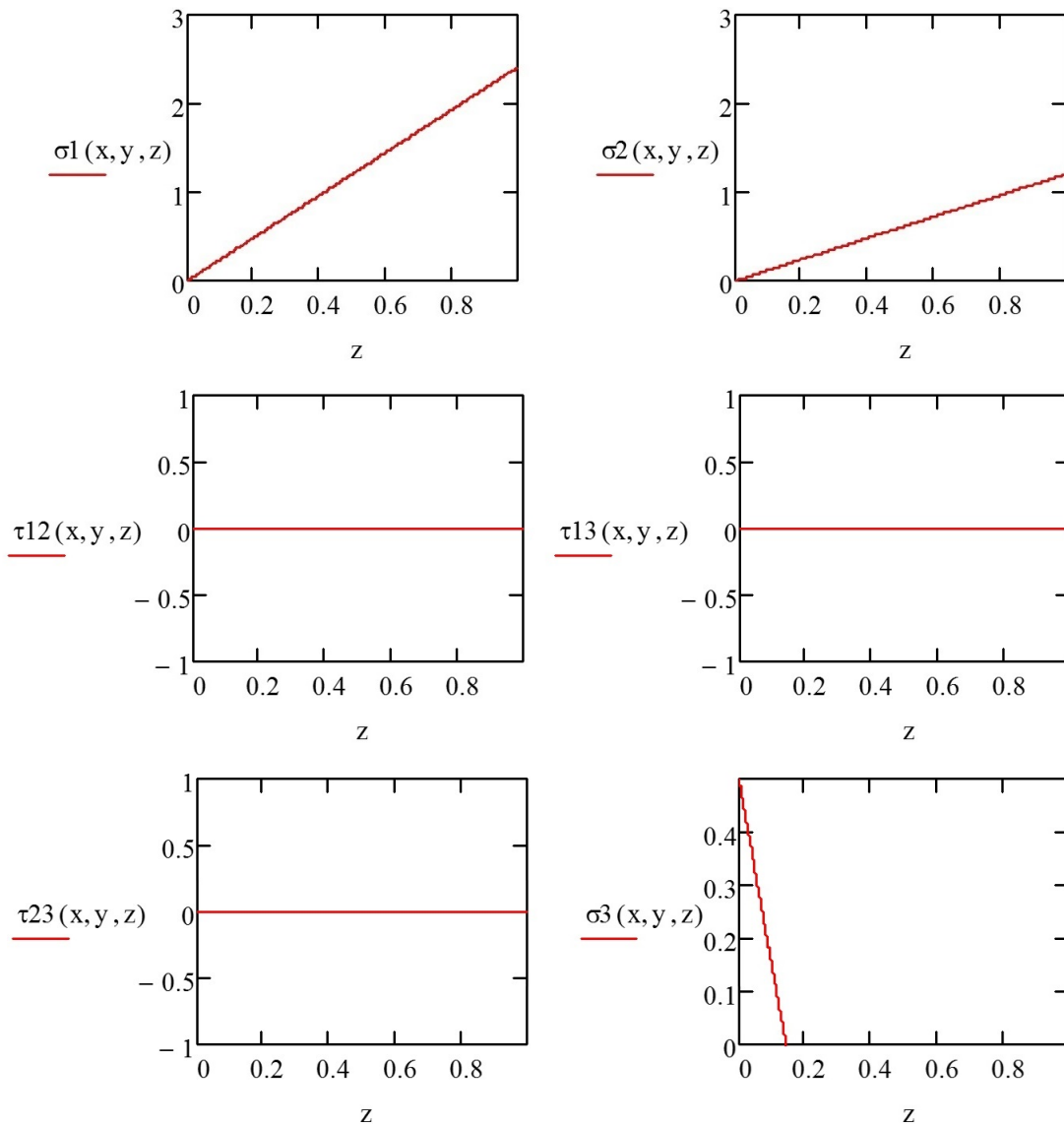


Figure 7. Stresses

Diagrams of the distribution functions (Fig. 8):

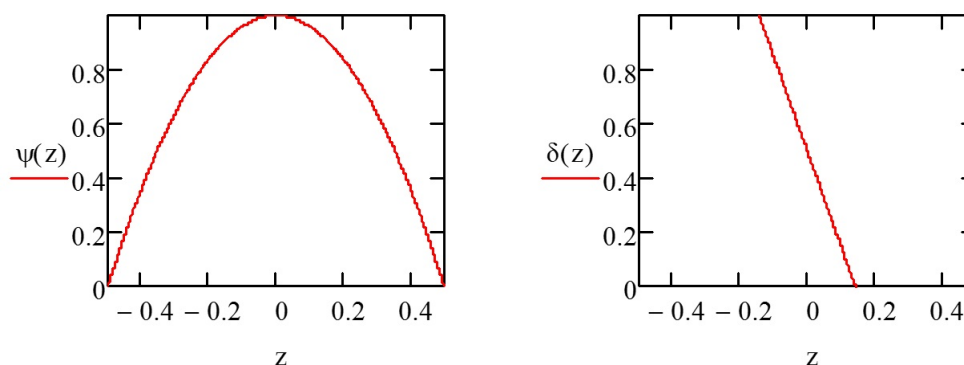


Figure 8. Distribution functions

The values of the distribution functions of the rigidly fixed elastic-plastic plate are given in Table 2 [17, 18].

Table 2

Values of distribution functions of the rigidly fixed elastic-plastic plate

$W(x, y, \xi)$	$U_1(x, y, z, \xi)$	$\varepsilon_1(x, y, z, \xi)$	$M_1(x, y)$	$M_{12}(x, y)$	$Q_1(x, y, \xi)$	$\sigma_1(x, y, z)$
0	0	0	-0.02	0	0	-0.469
$1.0068 \cdot 10^{-6}$	0	$-1.611 \cdot 10^{-5}$	$-3.922 \cdot 10^{-3}$	0	0.09	-0.094
$3.1820 \cdot 10^{-6}$	0	$-5.091 \cdot 10^{-5}$	0.015	0	0.12	0.365
$5.4815 \cdot 10^{-6}$	0	$-8.77 \cdot 10^{-5}$	0.033	0	0.105	0.783
$7.1595 \cdot 10^{-6}$	0	$-1.146 \cdot 10^{-4}$	0.045	0	0.06	1.07
$7.7685 \cdot 10^{-6}$	0	$-1.243 \cdot 10^{-4}$	0.049	0	0	1.172
$7.1595 \cdot 10^{-6}$	0	$-1.146 \cdot 10^{-4}$	0.045	0	-0.06	1.07
$5.4815 \cdot 10^{-6}$	0	$-8.77 \cdot 10^{-5}$	0.033	0	-0.105	0.783
$3.1820 \cdot 10^{-6}$	0	$-5.091 \cdot 10^{-5}$	0.015	0	-0.12	0.365
$1.0068 \cdot 10^{-6}$	0	$-1.611 \cdot 10^{-5}$	$-3.922 \cdot 10^{-3}$	0	-0.09	-0.094
0	0	0	-0.02	0	0	-0.469

Conclusions

Thus, this calculation was performed using elastic-plastic theory. The influence of the plate bending function in the form of polynomials in the elastic-plastic state is taken as a parameter. It is obtained analytically by applying the bending function of the beam taking into account the deformation. The law of change, which corresponds to the elastic-plastic material of stress, is used. In General, the calculation of the bending of a rigidly fixed elastic-plastic plate is shown.

It was found that many problems of the technique can be solved by the method of separating variables. Using this method simultaneously with the calculation of the plate bending, it is possible to solve the problem of free oscillations and other problems.

References

- 1 Liu M. Multiple fully stressed designs of steel frame structures with semi-rigid connections / M. Liu, S.A. Burns // International journal for numerical methods in engineering. — 2003. — Vol. 58, No. 6. — P. 821–838. DOI: 10.1002/nme.807.
- 2 Larsson D. In-plane modal testing of a free isotropic rectangular plate / D. Larsson // Experimental mechanics. — 1997. — Vol. 37, No. 3. — P. 339–343. DOI: 10.1007/BF02317428.
- 3 Турсунов К.А. Прямоугольный конечный элемент пластины / К.А. Турсунов, А.Е. Елешова // Тр. ун-та. Раздел Математика. Механика. — Караганда: Изд. КарГТУ, 2000. — Вып. 1(1). — С. 61–63.

- 4 Nuguzhinov Zh.S. Calculation of continuous beams taking into account the elastic compliance of supports / Zh.S. Nuguzhinov, S.K. Akhmediev, S.R. Zholmagambetov, O. Khabidolda // Bulletin of the Karaganda University. Mathematics series. — 2018. — No. 4 (92). — P. 139–147. DOI: 10.31489/2018M4/139-147
- 5 Yessenbayeva G.A. On the calculation of the rectangular finite element of the plate / G.A. Yessenbayeva, D.N. Yesbayeva, T.Kh. Makazhanova // Bulletin of the Karaganda University. Mathematics series. — 2018. — No. 2 (90). — P. 150–156. DOI: 10.31489/2018M2/150-156.
- 6 Kudaibergenov M.K. Stress-strain state horizontal coal seam of finite length / M.K. Kudaibergenov, A.L. Karchevsky, K.T. Iskakov // Bulletin of the Karaganda University. Mathematics series. — 2018. — No. 2 (90). — P. 133–142. DOI: 10.31489/2018M2/133-142.
- 7 Yessenbayeva G.A. On mathematical and analytical methods for solving problems on vibrations of membranes and plates / G.A. Yessenbayeva, D.N. Yesbayeva, D. Bauyrzhankyzy, D.A. Nurgali // Bulletin of the Karaganda University. Mathematics series. — 2018. — No. 1 (89). — P. 113–120.
- 8 He Z. Effect of vertex singularities on stress intensities near plate free surfaces / Z. He, A. Kotousov, F. Berto // Fatigue & Fracture of Engineering Materials & Structures. — 2015. — Vol. 38. — No. 7. — P. 860–869. DOI: 10.1111/ffe.12294.
- 9 Berto F. Three-dimensional effects in finite thickness plates weakened by rounded notches and holes under in-plane shear / F. Berto, C. Marangon // Fatigue & Fracture of Engineering Materials & Structures. — 2013. — Vol. 36. — No. 11. — P. 1139–1152. DOI: 10.1111/ffe.12098.
- 10 Campagnolo A. The effects of different boundary conditions on three-dimensional cracked discs under anti-plane loading / A. Campagnolo, F. Berto, P. Lazzarin // European Journal of Mechanics A-Solids. — 2015. — Vol. 50. — P. 76–86. DOI: 10.1016/j.euromechsol.2014.11.001.
- 11 Kotousov A. Effect of plate thickness on stress state at sharp notches and the strength paradox of thick plates / A. Kotousov // International Journal of Solids and Structures. — 2018. — Vol. 47. — No. 14–15. — P. 1916–1923. DOI: 10.1016/j.ijsolstr.2010.03.029.
- 12 Bambach M.R. Experimental techniques for testing unstiffened plates in compression and bending / M.R. Bambach, K.J.R. Rasmussen // Experimental mechanics. — 2004. — Vol. 44. — No. 1. — P. 91–96. DOI: 10.1177/0014485104039625.
- 13 Kotousov A. Fundamental solutions for the generalised plane strain theory / A. Kotousov, C.H. Wang // International Journal of Engineering Science. — 2002. — Vol. 40. — No. 15. — P. 1775–1790. DOI: 10.1016/S0020-7225(02)00041-1.
- 14 Kotousov A. Three-dimensional stress constraint in an elastic plate with a notch / A. Kotousov, C.H. Wang // International Journal of Solids and Structures. — 2002. — Vol. 39. — No. 16. — P. 4311–4326. DOI: 10.1016/S0020-7683(02)00340-2.
- 15 Lazzarin P. Three-dimensional stress fields due to notches in plates under linear elastic and elastic-plastic conditions / P. Lazzarin, M. Zappalorto, F. Berto // Fatigue & Fracture of Engineering Materials & Structures. — 2015. — Vol. 38. — No. 2. — P. 140–153. DOI: 10.1111/ffe.12138.
- 16 Nakamura T. 3-dimensional stress-field near the crack front of a thin elastic plate / T. Nakamura, D.M. Parks // Journal of Applied Mechanics-Transactions of the Asme. — 1988. — Vol. 55. — No. 4. — P. 805–813. DOI: 10.1115/1.3173725.
- 17 Beghini M. Measurement of coatings' elastic properties by mechanical methods: Part 1. Consideration on experimental errors / M. Beghini, L. Bertini, F. Frenzo // Experimental mechanics. — 2001. — Vol. 41. — No. 4. — P. 293–304. DOI: 10.1007/BF02323922.
- 18 Seytmuratov A.Zh. Equations of vibration of a two-dimensionally layered plate strictly based on the decision of various boundary-value problems / A.Zh. Seytmuratov, B.M. Nurlanova, N.K. Medeubaev // Bulletin of the Karaganda University. Mathematics series. — 2017. — No. 3 (87). — P. 109–116. DOI: 10.31489/2017M3/109-116.

Л.С. Әсетова, Б.М. Нурланова, И.А. Самойлова

Жақтары қатты бекітілген серпімді-ілімді пластинаның иілуі

Пластиналық конструкциялар қатарына жабулар, сонымен қатар тұтас кеңістіктік жүйе ретінде жұмыс істейтін қорап тәріздес жүйелер жатады. Пластиналық конструкциялар қатарына өзектер де, пластиналар да элементтер болып табылатын жүйелер кіреді, мысалы, каркасты-панельдік ғимараттардың көтеруші қабілеті бар белдік конструкциялар. Серпімді-ілімді пластинаның иілу теориясын қарастырғанда осы теория бойынша есептеу алгоритмі, оның неізгі формулалары, серпімділік теорияның неізгі қатыстары қарастырылды. Мақалада жақтары қатты бекітілген серпімді-ілімді пластинаның иілуі зерттелді. Есептеу айналымын бөлу әдісінің көмегімен жүргізілген. Бұл әдіс MathCAD бағдарламасы бойынша жүзеге асырылды. Кернеу мен материал модулінің функциясының өзгеру заңдарының мәндері, майысу функциясы, жылжулар компоненттері, деформация компоненттері, иілу, бұралу моменттері және ішкі күштер, кернеулердің мәндері алынды және үлестірім функцияларының эпюралары салынды. Жақтары қатты бекітілген серпімді-ілімді пластинаның таралу функцияларының мәндері анықталды.

Клт сөздер: пластина, серпімді, икемді, ілімді, иілу, деформация, кернеу.

Л.С. Асетова, Б.М. Нурланова, И.А. Самойлова

Изгиб жестко закрепленной упруго-пластической пластины

К числу пластинных конструкций относятся покрытия, а также коробчатые системы, работающие как целостная пространственная система. В состав пластинных конструкций входят системы, элементами которых являются как стержни, так и пластины, например, при рассмотрении теории изгиба это каркасно-панельные конструкции с несущей способностью каркасно-панельных зданий. В теории упруго-пластического изгиба пластин рассмотрены алгоритм расчета, его основные формулы, основные соотношения теории упругости. В статье рассчитан изгиб жестко закрепленной упруго-пластической пластины. Расчеты производились с помощью метода разделения переменных, реализованного с использованием программы MathCAD. Авторами получены значения законов изменения напряжений и функции модуля материалов, функции изгиба, компонентов сдвига и деформации, значения моментов изгиба, кручения и внутренних сил, напряжений. Построены эпюры функций распределения. Определены значения функций распределения жестко закрепленной упруго-пластической пластины.

Ключевые слова: пластина, упругий, пластический, податливость, изгиб, деформация, напряжение.

References

- 1 Liu, M., & Burns, S.A. (2003). Multiple fully stressed designs of steel frame structures with semi-rigid connections. *International journal for numerical methods in engineering*, Vol. 58, 6, 821–838. DOI: 10.1002/nme.807.
- 2 Larsson, D. (1997). In-plane modal testing of a free isotropic rectangular plate. *Experimental mechanics*, Vol. 37, 3, 339–343. DOI: 10.1007/BF02317428.
- 3 Tursunov, K.A., & Eleshova, A.E. (2000). Priamouholnyi konechnyi element plastiny [The rectangular finite plate element]. *Trudy universiteta. Razdel Matematika. Mekhanika – Proceedings of the University. Section: Mathematics. Mechanics. No 1(1)*, 61–63. Karaganda: Publ. KarHTU [in Russian].
- 4 Nuguzhinov, Zh.S., Akhmediev, S.K., Zholmagambetov, S.R., & Khabidolda O. (2018). Calculation of continuous beams taking into account the elastic compliance of supports. *Bulletin of the Karaganda University. Series Mathematics*, 4 (92), 139–147. DOI: 10.31489/2018M4/139-147.
- 5 Yessenbayeva, G.A., Yesbayeva, D.N., & Makazhanova, T.Kh. (2018). On the calculation of the rectangular finite element of the plate. *Bulletin of the Karaganda University. Mathematics series*, 2 (90), 150–156. DOI: 10.31489/2018M2/150-156.

- 6 Kudaibergenov, M.K., Karchevsky, A.L., & Iskakov, K.T. (2018). Stress-strain state horizontal coal seam of finite length. *Bulletin of the Karaganda University. Mathematics series*, 2 (90), 133–142. DOI: 10.31489 /2018M2/133-142.
- 7 Yessenbayeva, G.A., Yesbayeva, D.N., Bauyrzhankyzy, D., & Nurgali, D.A. (2018). On mathematical and analytical methods for solving problems on vibrations of membranes and plates. *Bulletin of the Karaganda University. Mathematics series*, 1 (89), 113–120.
- 8 He, Z., Kotousov, A., & Berto, F. (2015). Effect of vertex singularities on stress intensities near plate free surfaces. *Fatigue & Fracture of Engineering Materials & Structures*, Vol. 38, 7, 860–869. DOI: 10.1111/ffe.12294.
- 9 Berto, F., & Marangon, C. (2013). Three-dimensional effects in finite thickness plates weakened by rounded notches and holes under in-plane shear. *Fatigue & Fracture of Engineering Materials & Structures*, Vol. 36, 11, 1139–1152. DOI: 10.1111/ffe.12098.
- 10 Campagnolo, A., Berto, F., & Lazzarin, P. (2015). The effects of different boundary conditions on three-dimensional cracked discs under anti-plane loading. *European Journal of Mechanics A-Solids*, Vol. 50, 76–86. DOI: 10.1016/j.euromechsol.2014.11.001.
- 11 Kotousov, A. (2018). Effect of plate thickness on stress state at sharp notches and the strength paradox of thick plates. *International Journal of Solids and Structures*, Vol. 47, 14-15, 1916–1923. DOI: 10.1016/j.ijsolstr.2010.03.029.
- 12 Bambach, M.R., & Rasmussen, K.J.R. (2004). Experimental techniques for testing unstiffened plates in compression and bending. *Experimental mechanics*, Vol. 44, 1, 91–96. DOI: 10.1177/0014485104039625.
- 13 Kotousov, A., & Wang, C.H. (2002). Fundamental solutions for the generalised plane strain theory. *International Journal of Engineering Science*, Vol. 40, 15, 1775–1790. DOI: 10.1016/S0020-7225(02)00041-1.
- 14 Kotousov, A., & Wang, C.H. (2002). Three-dimensional stress constraint in an elastic plate with a notch. *International Journal of Solids and Structures*, Vol. 39, 16, 4311–4326. DOI: 10.1016/S0020-7683(02)00340-2.
- 15 Lazzarin, P., Zappalorto, M., & Berto, F. (2015). Three-dimensional stress fields due to notches in plates under linear elastic and elastic-plastic conditions. *Fatigue & Fracture of Engineering Materials & Structures*, Vol. 38, 2, 140–153. DOI: 10.1111/ffe.12138.
- 16 Nakamura, T., & Parks, D.M. (1988). 3-dimensional stress-field near the crack front of a thin elastic plate. *Journal of Applied Mechanics-Transactions of the Asme*, Vol. 55, 4, 805–813. DOI: 10.1115/1.3173725.
- 17 Beghini, M., Bertini, L., & Frenzo, F. (2001). Measurement of coatings' elastic properties by mechanical methods: Part 1. Consideration on experimental errors. *Experimental mechanics*, Vol. 41, 4, 293–304. DOI: 10.1007/BF02323922.
- 18 Seytmuratov, A.Zh., Nurlanova, B.M., & Medeubaev, N.K. (2017). Equations of vibration of a two-dimensionally layered plate strictly based on the decision of various boundary-value problems. *Bulletin of the Karaganda University. Mathematics series*, 33 (87), 109–116. DOI: 10.31489/2017M3/109-116.